# A multiclass cell transmission model for shared human and autonomous vehicle roads 

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## A R T I CLE INFO

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#### Abstract

Autonomous vehicles have the potential to improve link and intersection traffic behavior. Computer reaction times may admit reduced following headways and increase capacity and backwards wave speed. The degree of these improvements will depend on the proportion of autonomous vehicles in the network. To model arbitrary shared road scenarios, we develop a multiclass cell transmission model that admits variations in capacity and backwards wave speed in response to class proportions within each cell. The multiclass cell transmission model is shown to be consistent with the hydrodynamic theory. This paper then develops a car following model incorporating driver reaction time to predict capacity and backwards wave speed for multiclass scenarios. For intersection modeling, we adapt the legacy early method for intelligent traffic management (Bento et al., 2013) to general simulation-based dynamic traffic assignment models. Empirical results on a city network show that intersection controls are a major bottleneck in the model, and that the legacy early method improves over traffic signals when the autonomous vehicle proportion is sufficiently high.


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## 1. Introduction

Autonomous vehicle (AV) technology is rapidly maturing with testing permitted on public roads in several states. When AVs become available to the public, computer precision and communications may allow new behaviors to increase network capacity. For instance, Dresner and Stone (2004) proposed the tile-based reservation (TBR) intersection policy which reduces delay beyond optimized traffic signals (Fajardo et al., 2011). Besides offering new intersection behaviors, AVs may also increase link capacity because reduced reaction times requires smaller following distances, and AVs may be less affected than human-driven vehicles (HVs) by certain adverse road conditions. However, capacity improvements are complicated by sharing roads with HVs, which will likely be the case for many years before AVs are sufficiently available and affordable to be driven by all travelers.

TBR is compatible with shared roads (Dresner and Stone, 2007), and link behaviors may be performed safely with a mixed fleet of vehicles. However, modeling link and intersection capacity improvements from shared road policies is still an open problem. Most current models of AVs are micro-simulations, which are not computationally tractable for the traffic assignment typically used to determine route choice. Levin and Boyles (2015a) modified static link performance functions model to predict capacity improvements as a function of the proportion of AVs on each link based on Greenshields et al.,

[^0]1935Greenshields' (1935) capacity model. However, in reality the proportion of AVs on each link will vary over time. Dynamic traffic assignment (DTA) models flow more accurately than static models and can include the varying-time effects of capacity. Kesting et al. (2010) predicted theoretical capacity for adaptive cruise control and used linear regression to extrapolate for various proportions of connected vehicles (CVs) and non-CVs. For consistency with DTA, we use a constant acceleration model to analytically predict capacity and wave speed as a function of the proportion of each vehicle class on the road, and generalize to multiple classes with different reaction times. Whereas many previous papers on CVs use microsimulation experiments, we use DTA on a city network to study the impacts of AVs under dynamic user equilibrium (DUE) route choice.

This paper makes several contributions with the aim of developing a shared road DTA model: First, a multiclass cell transmission model (CTM) is proposed that admits space-time variations of capacity and wave speed. Second, a link capacity model based on a collision avoidance car following model with different reaction times is presented. The link capacity assumptions lead to the triangular fundamental diagram assumed by Newell (1993) and Yperman et al. (2005). To facilitate shared intersections, the conflict region (CR) algorithm from Levin and Boyles (2015b) for general SBDTA models is modified using Bento et al. (2013)'s control policy. Intersection efficiency scales dynamically with the proportion of AVs using the intersection. Results from studies on a single intersection and the downtown Austin city network suggest that travel time reductions when using reservation-based controls scale linearly with the proportion of AVs, but do not improve over signals until $80 \%$ AV penetration or greater.

The remainder of this paper is organized as follows. Section 2 discusses literature relevant to multiclass DTA and AV flow. Section 3 presents the multiclass DTA model and shows consistency with the hydrodynamic theory of traffic flow. Section 4 develops a dynamic capacity and wave speed model based on driver reaction times. A shared intersection model for general SBDTA is developed in Section 5. In Section 6, we present a case study on a city network involving varying levels of humandriven and autonomous vehicles, and Section 7 discusses conclusions.

## 2. Literature review

This literature review starts by discussing multiclass DTA in Section 2.1 to provide a context for the AV models discussed in Section 2.2.

### 2.1. Dynamic traffic assignment

DTA includes a number of different flow models, some of which are solved analytically and others which are simulationbased (SBDTA). For an overview of DTA, we refer to Chiu et al. (2011). This paper focuses on the cell transmission (CTM) SBDTA model (Daganzo, 1994, 1995a), which is a discrete approximation of the Lighthill-Whitham-Richards (LWR) model (Lighthill and Whitham, 1955; Richards, 1956). The partial differential equations of the LWR model are generally more difficult to solve when multiple vehicle classes result in varying capacities. However, the discretized space and time in CTM simplifies the multiclass solution method. The multiclass CTM presented in Section 3 is shown to be compatible with the conservation equations of LWR.

Multiclass DTA has previously been studied in the literature although primarily with a focus on heterogeneous vehicles of length and speed. Wong and Wong (2002) allowed vehicles to have a class-specific speed and demonstrate that their model adheres to flow conservation. However, they use a new discrete space-time approximation to solve their model, and it is not clear whether it is compatible with the most common simulation-based approximations, which is desirable for integration with existing DTA models. Tuerprasert and Aswakul (2010) formulated a multiclass CTM with different speeds per class, including how different speeds affect cell propagation. It is not clear, though, whether their model solves a multiclass form of LWR, or is a modification of CTM with useful properties.

### 2.2. Autonomous vehicle flow

The model presented in this paper is concerned with varying capacities and wave speeds due to the multiple classes of human-driven and autonomous vehicles. We assume that speed does not depend on vehicle class, which is reasonable because some AVs are programmed to exceed the speed limit to maintain the same speed as surrounding traffic (Miller, 2014) for improved safety (Aarts and Van Schagen, 2006).

Potential improvements in traffic flow from CVs and AVs have begun to receive attention in the literature. Adaptive cruise control (ACC) (Marsden et al., 2001) has been developed to improve link capacity and, if it is not incorporated into AVs, will likely influence AV car-following behavior. Van Arem et al. (2006) used a micro-simulation to show that cooperative ACC can improve efficiency. Kesting et al. (2010) developed a continuous acceleration behavior model of CVs to predict theoretical capacity. They use a linear regression to extrapolate for different proportions of CVs and non-CVs. We generalize by including multiple vehicle classes with different reaction times in our constant acceleration model and predict both capacity and wave speed as a function of the proportion of each vehicle class. Schakel et al. (2010) used simulation to study traffic flow stability, finding that ACC increases stability and also increases shockwave speed. This is consistent with the theoretical wave speed
we develop in Section 3. Although much of the literature uses micro-simulation to study CVs and AVs, we use the predicted capacities and wave speeds in a DTA model to study the impacts on a city network with DUE.

A major topic in the literature is new intersection policies for AVs. Dresner and Stone (2004) developed a reservationbased policy (TBR) using the greater precision and more complex communications possible with AVs. Fajardo et al. (2011) found that TBR improved over optimized traffic signals. Because TBR subsumes traffic signals, signals can be combined with an intersection agent controller to make TBR compatible with shared roads through an alternate reservationgranting policy (Dresner and Stone, 2007). Bento et al. (2013) proposed to extend TBR to non-communication equipped vehicles by reserving additional space to account for reduced precision and unknown destination, and Qian et al. (2014) developed a provably collision-free shared-intersection system. Other reservation prioritization policies with the goal of reducing intersection delay have been explored, such as intersection auctions (Schepperle and Bhm, 2007; Vasirani and Ossowski, 2012; Carlino et al., 2013). Analyzing TBR on city-size networks has been a major challenge as most AV traffic models have used micro-simulation. Carlino et al. (2012) used a simplified non-tile-based reservation policy to simulate a large network in reasonable time. However, the intersection capacity of this model was significantly reduced. Because of the number of simulations involved in solving DTA for user equilibrium, a micro-simulation model of intersections is not sufficient. Levin and Boyles (2015b) used a conflict region (CR) simplification to make TBR computationally tractable for DTA, and an extension of the CR model is used for intersections in this paper.

## 3. Multiclass cell transmission model

This section presents a multiclass extension of CTM. The focus of this paper is on for roads with both human and autonomous personal vehicles; we do not include the speed differences between heavy trucks and personal vehicles. The models in Sections 3 and 4 are defined for continuous flows, which some DTA models use. Because this paper is also concerned with node models, and because reservation-based intersection controls are defined for discrete vehicles, Sections 5 and 6 will discretize the flow model defined here. In this paper, we make the following assumptions.

1. All vehicles travel at the same speed. Although in reality vehicle speeds differ, in DTA models the vehicle speed behavior model is often assumed to be identical for all vehicles. This is reasonable even with multiple vehicle classes because AVs may match the speed of surrounding vehicles even if it requires exceeding the speed limit (Miller, 2014). Although Tuerprasert and Aswakul (2010) considered different vehicle speeds in CTM, in this study of HVs and AVs much of the differences in speed would come from variations in HV behavior that are often not considered in DTA models.
2. Uniform distribution of class-specific density per cell. Single-class CTM assumes the density within a cell is uniformly distributed. We extend that assumption to class-specific densities.
3. Arbitrary number of vehicle classes. Although this study focuses on the transition from HVs to AVs, different types of AVs may be certified for different reaction times, and thus may respond differently in their car-following behavior.
4. Backwards wave speed is less than or equal to free flow speed. This is necessary to determine cell length by free flow speed. Although this is a common assumption in DTA models, in Section 4 we show that a sufficiently low reaction time might break this assumption.

We first define the multiclass hydrodynamic theory in Section 3.1. Then, following the presentation of Daganzo (1994), we state the cell transition equations in Section 3.2 and show that they are consistent with the multiclass hydrodynamic theory in Section 3.3.

### 3.1. Multiclass hydrodynamic theory

Let $M$ be the set of vehicle classes. Let $k_{m}(x, t)$ be the density of vehicles of class $m$ at space-time point ( $x, t$ ) with total density denoted by $k(x, t)=\sum_{m \in M} k_{m}(x, t)$. Similarly, let $q_{m}(x, t)=u\left(\frac{k_{1}}{k}, \ldots, \frac{k_{M}}{k}\right) k_{m}(x, t)$ be the class-specific flow, with the total flow given by $q(x, t)=\sum_{m \in M} q_{m}(x, t)$, and let the function $u\left(\frac{k_{1}}{k}, \ldots, \frac{k_{M}}{k}\right)$ denote the speed possible with class proportions of $\frac{k_{1}}{k}, \ldots, \frac{k_{|M|}}{k}$.

Speed is limited by free flow speed, capacity, and backwards wave propagation:

$$
\begin{equation*}
u\left(k_{1}, \ldots k_{|M|}\right)=\min \left\{u^{\mathrm{f}}, \frac{\left.q^{\max \left(\frac{k_{1}}{k}\right.}, \ldots, \frac{k_{M \mid}}{k}\right)}{k}, w\left(\frac{k_{1}}{k}, \ldots, \frac{k_{|M|}}{k}\right) \frac{k^{\mathrm{jam}}-k}{k}\right\} \tag{1}
\end{equation*}
$$

where $u^{\mathrm{f}}$ is free flow speed, $w\left(\frac{k_{1}}{k}, \ldots, \frac{k_{M}}{k}\right)$ is the backwards wave speed, $q^{\max }\left(\frac{k_{1}}{k}, \ldots, \frac{k_{M}}{k}\right)$ is the capacity when the proportions of density in each class are $\frac{k_{1}}{k}, \ldots, \frac{k_{|M|}}{k}$, and $k^{\mathrm{jam}}$ is jam density. $k^{\mathrm{jam}}$ is assumed not to depend on vehicle type, as the physical characteristics (such as length and maximum acceleration) of human-driven and autonomous vehicles are assumed to be the same. For consistency, conservation of flow must be satisfied, i.e. $\frac{\partial q_{m}(x, t)}{\partial x}=-\frac{\partial k_{m}(x, t)}{\partial t}$ for all $m \in M$ (Wong and Wong, 2002).

### 3.2. Cell transition flows

As with Daganzo (1994), to form the multiclass CTM we discretize time into timesteps of $d t$. Links are then discretized into cells labeled by $i=1, I$ such that vehicles traveling at free flow speed will travel exactly the distance of one cell per timestep. Let $n_{i}^{m}(t)$ be vehicles of class $m$ in cell $i$ at time $t$, where $n_{i}(t)=\sum_{m \in M} n_{i}^{m}(t)$. Let $y_{i}^{m}(t)$ be vehicles of class $m$ entering cell $i$ from cell $i-1$ at time $t$. Then cell occupancy is defined by

$$
\begin{equation*}
n_{i}^{m}(t+1)=n_{i}^{m}(t)+y_{i}^{m}(t)-y_{i+1}^{m}(t) \tag{2}
\end{equation*}
$$

with total transition flows given by

$$
\begin{equation*}
y_{i}(t)=\sum_{m \in M} y_{i}^{m}(t)=\min \left\{\sum_{m \in M} n_{i-1}^{m}(t), Q_{i}(t), \frac{w_{i}(t)}{u^{\mathrm{f}}}\left(N-\sum_{m \in M} n_{i}^{m}(t)\right)\right\} \tag{3}
\end{equation*}
$$

where $N$ is the maximum number of vehicles that can fit in cell $i$ and $Q_{i}(t)$ is the maximum flow.
Eq. (3) defines the total transition flows, which will now be defined specific to vehicle class. To avoid dividing by zero, assume $n_{i-1}(t)>0$. (If $n_{i-1}(t)=0$, there is no flow to propagate). As stated in Assumption 2, class-specific density is assumed to be uniformly distributed throughout the cell. Then class-specific transition flows are proportional to $\frac{n_{i-1}^{m}(t)}{n_{i-1}(t)}$ :

$$
\begin{equation*}
y_{i}^{m}(t)=\frac{n_{i-1}^{m}(t)}{n_{i-1}(t)} \min \left\{\sum_{m \in M} n_{i-1}^{m}(t), Q_{i}(t), \frac{w_{i}(t)}{u^{\mathrm{f}}}\left(N-\sum_{m \in M} n_{i}^{m}(t)\right)\right\} \tag{4}
\end{equation*}
$$

Eq. (4) may be simplified to

$$
\begin{equation*}
y_{i}^{m}(t)=\min \left\{n_{i-1}^{m}(t), \frac{n_{i-1}^{m}(t)}{n_{i-1}(t)} Q_{i}(t), \frac{n_{i-1}^{m}(t)}{n_{i-1}(t)} \frac{w_{i}(t)}{u^{\mathrm{f}}}\left(N-\sum_{m \in M} n_{i}^{m}(t)\right)\right\} \tag{5}
\end{equation*}
$$

which shows that flow of class $m$ is restricted by three factors: (1) class-specific cell occupancy; (2) proportional share of the capacity; and (3) proportional share of congested flow.

In the general hydrodynamic theory, class proportions may vary arbitrarily with space and time, which includes the possibility of variations within a cell. Therefore, assuming uniformly distributed density results in the possibility of non-FIFO behavior within cells. One class may have a higher proportion at the end of the cell, and thus might be expected to comprise a higher proportion of the transition flow. However, as discussed by Blumberg and Bar-Gera (2009), even single class CTMs may violate FIFO. The numerical experiments in this paper use discretized flow to admit reservation-based intersection models. The discretized flow also allows vehicles within a cell to be contained within a FIFO queue, which ensures FIFO behavior at the cell level. Total transition flows for discrete vehicles are determined as stated above for continuous flow.

### 3.3. Consistency with hydrodynamic theory

As with Daganzo (1994) we show that these transition flows are consistent with the multiclass hydrodynamic theory defined in Section 3.1. Assume class-specific flow is proportional to density, i.e. $\frac{k_{m}}{k}$, and all classes travel at the same speed. Also assume that $k>0$, because if $k=0$ then flow is also 0 . Then

$$
\begin{equation*}
q_{m}(x, t)=\frac{k_{m}}{k} \min \left\{u^{\mathrm{f}} k, q^{\max }\left(\frac{k_{1}}{k}, \ldots, \frac{k_{|M|}}{k}\right), w\left(\frac{k_{1}}{k}, \ldots, \frac{k_{|M|}}{k}\right)\left(k^{\mathrm{jam}}-k\right)\right\} \tag{6}
\end{equation*}
$$

Let $d t$ be the timestep and choose cell length such that $u^{\mathrm{f}} \cdot d t=1$. Then cell length is 1 , $u^{\mathrm{f}}$ is 1 , $x=i, k^{\mathrm{jam}}=N, q^{\max }(t)=Q(t)$, and $k(x, t)=n_{i}(t)$. Cell length is chosen so that flow may traverse at most one cell per timestep to satisfy the Courant-Friedrichs-Lewy condition (Courant et al., 1928). Then

$$
\begin{equation*}
q_{m}(x, t)=\frac{n_{i}^{m}(t)}{n_{i}(t)} \min \left\{n_{i}(t), q_{i}^{\max }(t), \frac{w_{i}(t)}{v}\left(N-n_{i}(t)\right)\right\}=y_{i+1}^{m}(t) \tag{7}
\end{equation*}
$$

except for the subindex of $n$ the last term, which should be $i+1$. As with Daganzo (1994) this difference is disregarded. (See Daganzo, 1995b for more discussion on this issue.) Therefore $\frac{\partial q_{m}(x, t)}{\partial x}=y_{i+1}^{m}(t)-y_{i}^{m}(t)$. Since $\frac{\partial k_{m}(x, t)}{\partial t}=n_{i}^{m}(t+1)-n_{i}^{m}(t)$ is the rate of change in cell occupancy with respect to time, the conservation of flow equation $\frac{\partial q_{m}(x, t)}{\partial x}=-\frac{\partial k_{m}(x, t)}{\partial t}$ is satisfied by the cell propagation function of Eq. (2).

## 4. Link capacity and backwards wave speed

We now present a car following model based on kinematics to predict the speed-density relationship as a function of the reaction times of multiple classes. Car following models can be divided into several types as described by Brackstone and McDonald, 1999 and Gartner et al. (2005). For instance, some predict fluctuations in the acceleration behavior of an
individual driver in response to the vehicle ahead. However, for DTA a simpler model is more appropriate to predict the speed of traffic at a macroscopic level. Newell (2002) greatly simplified car following to be consistent with the hydrodynamic theory, but the model does not include the effects of reaction time. Instead, the car following model used here builds from the collision avoidance theory of Kometani and Sasaki (1959) to predict the allowed headway for a given speed, which varies with driver reaction time. The inverse relationship predicts speed as a function of the headway, which is determined by density. This car following model results in the triangular fundamental diagram used by Newell (1993) and Yperman et al. (2005).

Although this car following model is useful in predicting the effects of a heterogeneous vehicle composition on capacity and wave speed, other effects such as roadway conditions are not included. Furthermore, CTM assumes a trapezoidal fundamental diagram that admits a lower restriction on capacity. Therefore, the effect of reaction times on capacity and backwards wave speed are used to appropriately scale link characteristics for realistic city network models. Although AVs may be less affected by adverse roadway conditions than human drivers, this paper assumes similar effects for the purposes of developing a DTA model of shared roads. Other estimations of capacity and wave speed may also be included in the multiclass CTM model developed in Section 3.

### 4.1. Safe following distance

Suppose that vehicle 2 follows vehicle 1 at speed $u$ with vehicle lengths $\ell$. Vehicle 1 decelerates at $a$ to a full stop starting at time $t=0$, and vehicle 2 follows suit after a reaction time of $\Delta t$. The safe following distance, $L$, is determined by kinematics.

The position of vehicle 1 is given by

$$
x_{1}(t)= \begin{cases}u t-\frac{1}{2} a t^{2} & t \leqslant \frac{u}{a}  \tag{8}\\ \frac{u^{2}}{2 a} & t>\frac{u}{a}\end{cases}
$$

where $\frac{u}{a}$ is the time required to reach a full stop. For $t>\frac{u}{a}$, the position of vehicle 1 is constant after its full stop. The position of vehicle 2 , including the following distance of $L$, is

$$
x_{2}(t)= \begin{cases}u t-L & t \leqslant \Delta t  \tag{9}\\ u t-\frac{1}{2} a(t-\Delta t)^{2}-L & t>\Delta t\end{cases}
$$

The difference is

$$
x_{1}(t)-x_{2}(t)= \begin{cases}u-\frac{1}{2} a t^{2}+L & t \leqslant \Delta t  \tag{10}\\ -a t \Delta t+\frac{1}{2} a(\Delta t)^{2}+L & \Delta t<t \leqslant \frac{u}{a} \\ \frac{u^{2}}{2 a}-u t+\frac{1}{2} a(t-\Delta t)^{2}+L & t>\frac{u}{a}\end{cases}
$$

and the minimum distance occurs when both vehicles are stopped, at $\frac{u}{a}+\Delta t$. To avoid a collision,

$$
\begin{equation*}
L \geqslant-\frac{u^{2}}{2 a}+u\left(\frac{u}{a}+\Delta t\right)-\frac{1}{2} a\left(\frac{u}{a}\right)^{2}+\ell=u \Delta t+\ell \tag{11}
\end{equation*}
$$

### 4.2. Flow-density relationship

Equivalently, Eq. (11) may be expressed as

$$
\begin{equation*}
u \leqslant \frac{L-\ell}{\Delta t} \tag{12}
\end{equation*}
$$

which restricts speed based on following distance (from density). Flow may be determined from the relationship $q=\left(\frac{L-\ell}{\Delta t}\right) k$ with $L=\frac{1}{k}$, which is linear with respect to density. Fig. 1 shows the resulting relationship between flow and density for different reaction times for a characteristic vehicle of length 20 feet that decelerates at 9 feet per second for a free flow speed of 60 miles per hour. Since speed is bounded by free flow speed and available following distance, the triangle is formed by $q=\min \left\{u k,\left(\frac{L-\ell}{\Delta t}\right) k\right\}$. Reaction times of 1 to 1.5 s correspond to human drivers (Johansson and Rumar, 1971).

The maximum density at which a speed of $u$ is possible is $\frac{1}{u \Delta t+\ell}$ from Eq. (12), and therefore capacity for free flow speed of $u^{f}$ is

$$
\begin{equation*}
q^{\max }=u^{\mathrm{f}} \frac{1}{u^{\mathrm{f}} \Delta t+\ell} \tag{13}
\end{equation*}
$$

Backwards wave speed is

$$
\begin{equation*}
w=-\frac{\frac{u^{\mathrm{f}}}{u^{\mathrm{f}} \Delta t+\ell}}{\frac{1}{u^{\mathrm{t} \Delta t+\ell}}-\frac{1}{\ell}}=\frac{\ell}{\Delta t} \tag{14}
\end{equation*}
$$



Fig. 1. Flow-density relationship as a function of reaction time.
which increases as reaction time decreases. The direction of this relationship is consistent with micro-simulation results by Schakel et al. (2010). Note that if $\Delta t<\frac{\ell}{u^{t}}$, which may be possible for computer reaction times, then backwards wave speed exceeds free flow speed. If $w>u^{\mathrm{f}}$ for CTM, then the cell lengths would need to be derived from the backward wave speed, not the forward. That would complicate the cell transition flows. To avoid this issue, this paper assumes that $w \leqslant u^{\mathrm{f}}$.

### 4.3. Flow for heterogeneous vehicles

The car following model in Section 4.2 is designed to estimate the capacity and backwards wave speed when the reaction time varies, but is uniform across all vehicles. This section expands the model for heterogeneous flow with different vehicles having different reaction times. Let the density be disaggregated into $k_{m}$ for each vehicle class $m$. Consider the case where speed is limited by density. Assuming that all vehicles travel at the same speed, for all vehicle classes,

$$
\begin{equation*}
u=\frac{L_{m}-\ell}{\Delta t_{m}} \tag{15}
\end{equation*}
$$

where $L_{m}$ is the headway allotted and $\Delta t_{m}$ is the reaction time for vehicles of class $m$. Also, with appropriate units,

$$
\begin{equation*}
\sum_{m \in M} k_{m} L_{m}=1 \tag{16}
\end{equation*}
$$

is the total distance occupied by the vehicles. Thus

$$
\begin{equation*}
\sum_{m \in M} k_{m}\left(L_{m}-\ell\right)=1-k \ell \tag{17}
\end{equation*}
$$

By Eq. (15), $\sum_{m \in M} k_{m} u \Delta t_{m}=1-k \ell$, and

$$
\begin{equation*}
u=\frac{1-k \ell}{\sum_{m \in M} k_{m} \Delta t_{m}} \tag{18}
\end{equation*}
$$

Eq. (18) may be rewritten as $u \sum_{m \in M} k_{m} \Delta t_{m}=1-k \ell$. Dividing both sides by $k$ yields

$$
\begin{equation*}
u \sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}+\ell=\frac{1}{k} \tag{19}
\end{equation*}
$$

Assuming that vehicle class proportions $\frac{k_{m}}{k}$ remain constant because all vehicles travel at the same speed, the maximum density for which a speed of $u^{\mathrm{f}}$ is possible is

$$
\begin{equation*}
k=\frac{1}{u^{\mathrm{f}} \sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}+\ell} \tag{20}
\end{equation*}
$$

which follows by taking the reciprocal of Eq. (19). Capacity is

$$
\begin{equation*}
q^{\max }=u^{\mathrm{f}} \frac{1}{u^{\mathrm{f}} \sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}+\ell} \tag{21}
\end{equation*}
$$

Backwards wave speed is thus

$$
\begin{equation*}
w=-\frac{\frac{u^{\mathrm{f}}}{u^{\mathrm{f}} \sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}+\ell}}{\frac{u^{\mathrm{f}} \sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}+\ell}{}-\frac{1}{\ell}}=\frac{\ell}{\sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}} \tag{22}
\end{equation*}
$$

Eqs. (18)-(22) reduce to the model in Section 4.2 in the single vehicle class scenario. Fig. 2 shows an example of how capacity and wave speed increase as the $A V$ proportion increases when human drivers have a reaction time of 1 s and autonomous vehicles have a reaction time of 0.5 s . The cases of $0 \%$ AVs and $100 \%$ AVs are identical to the 1 s reaction time and 0.5 s reaction time fundamental diagrams in Fig. 1, respectively.

### 4.4. Other factors affecting capacity

In reality, factors such as narrow lanes and road conditions affect capacity as well. These factors are usually in Highway Capacity Manual estimates of roadway capacity used for city network models. The model above, however, does not include factors beyond speed limit. To include these factors in the experimental results in Section 5, we scale existing estimates on capacity and wave speed in accordance with Eqs. (21) and (22). Although the model in Section 4.3 predicts a triangular fundamental diagram as used by Newell (1993) and Yperman et al. (2005), other flow-density relationships are often used. CTM, the basis for multiclass DTA in this paper, uses a trapezoidal fundamental diagram.

Assume estimated roadway capacity and wave speed are $\hat{q}^{\max }$ and $\hat{w}$, respectively, and that the reaction time for human drivers is $\Delta t_{\mathrm{HV}}$. Human reaction times may vary depending on the location of the road; for instance reaction times on rural roads are often greater than those in the city. Because capacity is affected by reaction time through Eq. (21), scaled capacity $\tilde{q}^{\max }$ is

$$
\begin{equation*}
\tilde{q}^{\max }=\frac{u^{\mathrm{f}} \Delta t_{\mathrm{HV}}+\ell}{u^{\mathrm{f}} \sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}+\ell} \hat{q}^{\max } \tag{23}
\end{equation*}
$$

Similarly, wave speed is affected by reaction time through Eq. (22), so scaled wave speed $\tilde{w}$ is

$$
\begin{equation*}
\tilde{w}=\frac{\Delta t_{\mathrm{HV}}}{\sum_{m \in M} \frac{k_{m}}{k} \Delta t_{m}} \hat{w} \tag{24}
\end{equation*}
$$

Eqs. (23) and (24) provide a method to integrate the capacity and backwards wave speed scaling of Section 4.3 with other factors and realistic data.

## 5. Intersection control policy

For shared road models, the intersection control policy is an important question. With $100 \%$ human vehicles, optimized traffic signals are the best option available. With $100 \%$ AVs, TBR can reduce delay beyond that of optimized signals (Fajardo et al., 2011). The difficulty is the choice of intersection control policy for shared roads. Dresner and Stone (2007) showed that TBR subsumes traffic signals because the signal essentially reserves parts of the intersection. They propose link- and lanecycling signals, where each link or lane successively receives full access to the intersection, and vehicles in other links or lanes may reserve non-conflicting paths. However, blocking out large portions of the intersection for a signal greatly restricts reservations from other links due to the possibility of conflict, even when most vehicles are AVs. As a result, this may not scale well when the proportion of AVs on the road becomes large. It is also an open question whether link- or lanecycling signals even outperform optimized traffic signals.


Fig. 2. Flow-density relationship as a function of $A V$ proportion.

Bento et al. (2013) proposed the legacy early method for intelligent traffic management (LEMITM) policy of reserving space-time for all possible turning movements and increasing the safety margins for non-AVs to allow them to use the TBR infrastructure. AVs still use conventional TBR, reserving only the requested path. This may be less efficient than traffic signals at small proportions of AVs because of the extra space-time reserved to ensure safety. However, as the proportion of AVs increases, TBR/LEMITM will devote less space-time to safety of human vehicles because it is not constrained by protecting turning movements allowed by traffic signals. As a result, TBR/LEMITM may scale at a higher rate. Therefore, TBR/ LEMITM is used in this paper to study how link and intersection capacity scales with the proportion of AVs.

TBR/LEMITM makes two assumptions that we elaborate on here for the purposes of describing the DTA model of TBR/ LEMITM. First, it separates vehicles into two groups: those that can establish digital communications on reservation acceptance and adherence, and those that cannot. The latter group consists of all non-AVs, although some AVs could conceivably fall into that group as well. This is possible in practice because current technology can already determine whether a vehicle is waiting at the intersection for actuated signals. Given that a vehicle is waiting, the intersection controller need only check whether the vehicle has established digital communications, which can be determined if vehicles transmit their position to the intersection controller along with reservation requests. Second, due to the unpredictably of human behavior, the intersection controller must be able to cancel granted reservations for AVs if a human is delayed in reacting to permission to enter the intersection. Because this DTA model does not include potential human errors and takes a more aggregate view of the intersection, canceled reservations are not included in the model.

Most studies on reservation-based controls use micro-simulation and are therefore not computationally tractable for the number of simulations required to solve DTA. Levin and Boyles (2015b) simplified TBR using the idea of larger conflict regions (CR) to distribute intersection capacity and receiving flows to sending flows for compatibility with general SBDTA models. Although the CR model is designed for arbitrary vehicle prioritization, TBR/LEMITM requires the intersection controller to reserve additional space and therefore make additional availability checks. Section 5.1 details the modifications to the CR algorithm to accommodate TBR/LEMITM.

### 5.1. Modified conflict region model

The conflict region model is a polynomial-time algorithm performed at each intersection each timestep to determine intersection movement. Vehicle movement is restricted by capacity of each conflict region it passes through during its turning movement. The purpose of the conflict region algorithm (Algorithms $1 \& 2$ ) is to determine which vehicles move subject to the constraints of sending flow, receiving flow, and conflict region capacity. The development of the conflict region algorithm is described in greater detail by Levin and Boyles (2015b). This section focuses on the modifications necessary to implement LEMITM.

The conflict region model requires discretized flow because of the priority function. For instance, Dresner and Stone (2004) propose a first-come-first-serve priority, and Dresner and Stone (2006) suggest priority for emergency vehicles. Modeling such prioritization functions with continuous flow is an open question, so discretized flow is used instead. These prioritization functions are orthogonal to the TBR/LEMITM control policy, although the communications required for more complex prioritization functions such as auctions may be difficult for human drivers.

Let $\Gamma^{-1}$ be the set of incoming links and $\Gamma$ be the set of outgoing links for the intersection. The intersection is divided into a set of non-overlapping conflict regions $C$, with $C_{i j}$ the subset of $C$ through which vehicles turning from $i \in \Gamma^{-1}$ to $j \in \Gamma$ will pass. Let $y_{i j}(t)$ be the number of vehicles that have moved from $i$ to $j$ and $y_{c}$ be the equivalent flow that has entered conflict region $c$ in timestep $t$. Let $Q_{i}$ be the capacity of link $i$ and $Q_{i j}=\min \left\{Q_{i}, Q_{j}\right\}$ be the capacity of the turning movement from $i$ to $j$. Every conflict region has some capacity

$$
\begin{equation*}
Q_{c}=\max _{(i, j) \mid c \in C_{i j}}\left\{Q_{i j}\right\} \tag{25}
\end{equation*}
$$

to allow flow of $\min \left\{Q_{i}, Q_{j}\right\}$ for any $(i, j)$ such that $c \in C_{i j}$ if no other demand is present, and vehicles traveling from $i$ to $j$ consume $\frac{Q_{c}}{Q_{i j}}$ of the capacity of $c \frac{Q_{c}}{Q_{i j}}>1$ refers to the case in which a vehicle from one approach reserves a capacity equivalent to more than 1 vehicle from another approach. For example, in a local road-arterial intersection, 1 vehicle crossing the intersection from the local road might prevent 2 vehicles on the arterial from moving.

Let $l_{i}$ be the number of lanes and $S_{i}(t)$ the sending flow of link $i$ at time $t$, i.e. the set of vehicles that could leave $i$ at t if no other constraints were present. Each vehicle $v$ has some priority defined by the arbitrary function $f(v, i)$. Let $R_{j}(t)$ be the receiving flow of link $j$, i.e. the number of vehicles that could enter $j$ at $t$ if incoming flow was infinite. Sending and receiving flows are general characteristics of dynamic flow models and allow the CR model to be applied to general SBDTA models. Denote by $\delta_{v}^{\mathrm{AV}}$ whether vehicle $v$ is autonomous.

Two modifications to the control algorithm are required to implement TBR/LEMITM. First, for non-AVs, movement from $i$ to $j$ across the intersection requires available capacity for all possible turning movements from $i$ because the vehicle cannot communicate its destination to the intersection controller. The set of conflict regions a vehicle leaving link $i$ could pass through is $\cup_{j^{\prime} \in \Gamma} C_{i j^{\prime}}$. It is not specific to $j$ because for a human vehicle, the intersection manager does not know the vehicle's destination link. Therefore the intersection controller must check whether all such turning movements have space available.

Second, when such a reservation is accepted, space for all possible turning movements from $i$ must be reserved. The modified CR model is formalized in Algorithms 1 \& 2.

Algorithm 1. Conflict region algorithm (see Algorithm 2 for canMove procedure)

```
Set \(V=\emptyset\)
for all \(i \in \Gamma^{-1}\) do
    Sort \(S_{i}(t)\) by arrival time at \(i\)
    Remove first \(l_{i}\) vehicles in \(S_{i}(t)\) and add them to \(V\)
    for all \(j \in \Gamma\) do
            Set \(y_{i j}(t)=0\)
    end for
    end for
    Sort \(V\) by \(f(v)\)
    for all \(v \in V\) do
        Let \((i, j)\) be the turning movement of \(v\)
        if canMove \(\left(\delta_{v}^{\mathrm{AV}}, i, j\right)\) then
            Set \(y_{i j}(t)=y_{i j}(t)+1\)
            if \(\delta_{v}^{\mathrm{AV}}=1\) then
                for all \(c \in C_{i j}\) do
                    Set \(y_{c}(t)=y_{c}(t)+\frac{Q_{c}}{Q_{i} j}\)
                end for
            else
                for all \(c \in \cup_{j^{\prime} \in \Gamma} C_{i j^{\prime}}\) do
                    Set \(y_{c}(t)=y_{c}(t)+\frac{Q_{c}}{Q_{i} j}\)
                end for
            end if
            Remove next vehicle in \(S_{i}(t)\) and add it to \(V\) in sorted order
            Go to line 10
        end if
    end for
```


## Algorithm 2. canMove procedure

```
function canMove \(\left(\delta_{v}^{\mathrm{AV}}, i \in \Gamma^{-1}, j \in \Gamma\right)\)
    if \(R_{j}-\sum_{i^{\prime} \in \Gamma^{-1}} y_{i^{\prime} j}(t)<\frac{u_{i}^{f} \Delta t_{\nu}+\ell}{u_{i}^{i} \Delta t_{\mathrm{HV}}+\ell}\) then
        Return False
    end if
    if \(\delta_{v}^{\mathrm{AV}}=1\) then
            for all \(c \in C_{i j}\) do
                if \(Q_{c}-y_{c}(t)<\frac{u_{i}^{f} \Delta t_{v}+\ell}{u_{i}^{i} \Delta t_{\mathrm{Hv}}+\ell} \frac{Q_{c}}{Q_{i j}}\) then
                Return False
                end if
            end for
        else
            for all \(c \in \cup_{j^{\prime} \in \Gamma} C_{i j^{\prime}}\) do
                if \(Q_{c}-y_{c}(t)<\frac{u_{i}^{i} \Delta t_{v}+\ell}{u_{i}^{i} \Delta t_{\mathrm{HV}}+\ell} Q_{c} Q_{\mathrm{ij}} t\) then
                    Return False
                end if
            end for
        end if
        Return True
    end function
```


### 5.2. Adjusted flows for vehicle classes

As shown in Section 4, cell capacities can be adjusted based on the reaction times of vehicles in the cell. However, CR capacities cannot similarly be adjusted because it is not known in advance which vehicles will pass through. Instead, the equivalent flow is adjusted based on the vehicle reaction time. Levin and Boyles (2015b) adjust the equivalent flow to account for differences in speeds from incoming links. Here we define an adjustment to equivalent flow because of differences in density due to reaction times. Vehicles with lower reaction times consume a smaller amount of the capacity. Based on Eq. (23), when the base capacity $\hat{q}^{\max }$ is used to determine CR capacity, a vehicle $v$ with reaction time $\Delta t_{v}$ should have an equivalent flow of

$$
\begin{equation*}
\frac{u_{i}^{\mathrm{f}} \Delta t_{v}+\ell}{u_{i}^{\mathrm{f}} \Delta t_{\mathrm{HV}}+\ell} \tag{26}
\end{equation*}
$$

where $u_{i}^{\mathrm{f}}$ is the free flow speed of link $i$.

## 6. Experimental results

This section describes the results of two experiments using multiclass CTM and TBR/LEMITM. All experiments used a custom DTA software implemented in Java. First we study a single intersection to determine how TBR/LEMITM affects intersection delay as the proportion of AVs increases. Second, we implement the shared road model in DTA on the downtown Austin city network with varying proportions of AVs to study the effects on total travel time and compare with traffic signals. Although TBR/LEMITM was introduced by Bento et al. (2013), their experiments are focused on the efficiency of the various intersection controls they study rather than their use in combination. Therefore the experiments in this section are a first look at using TBR/LEMITM as needed in a shared road scenario. These are also the first results for shared roads with DUE routing behavior.

For these experiments, flow is discretized so reservation-based intersection controls may be used. As a result, vehicles within a cell are contained in a FIFO queue, and FIFO is ensured within cells except at intersections. Cell transition flows are restricted by capacity and cell density as functions of class proportions as discussed in Sections 3 and 4.

To study a gradual shift from HVs to AVs, flow is separated into two classes: HVs with a reaction time of 1 s , and AVs with a reaction time of $0.5 \mathrm{~s} . \ell$ is 20 feet for the purposes of car following and jam density. The experiments hold the total demand fixed while changing the proportion of AVs. Based on Eq. (26), with the parameters of this study, AVs require 0.593 of the capacity that HVs require. The vehicular demand places, on average, $1400\left(p^{\mathrm{HV}}+0.593 p^{\mathrm{AV}}\right)+1300\left(p^{\mathrm{HV}}\right)$ vehicles per hour demand on the intersection in each direction.

### 6.1. Single intersection

First, we study the four link, single lane intersection shown in Fig. 3 with capacity and demand chosen to demonstrate two observed conditions for the effects of TBR/LEMITM on single intersections. Each approach has demand of 1200 vehicles


Fig. 3. Single intersection case study.


Fig. 4. Average travel time per vehicle at different proportions of AVs.
per hour through traffic, 200 vehicles per hour right-turning, and 100 vehicles per hour left-turning traffic. Each link is 1 mile long and has capacity of 1800 vehicles per hour, which does not allow all demand to be satisfied on average when a significant proportion of vehicles are HVs. Links have a free flow speed of 60 miles per hour and a backwards wave speed of half the free flow speed - 30 miles per hour. Capacity and backwards wave speed increase with the proportion of AVs as defined in Section 4.4.

Experiments were performed at $10 \%$ intervals of AV proportion. Each experiment had 1 hour of demand with vehicle departure times randomly chosen. Experiments were repeated 10 times and average travel times per vehicle are shown in Fig. 3. Between $0 \%$ and $60 \%$ AVs, average travel time decreases linearly with the proportion of AVs. Between $70 \%$ and $100 \%$ AVs, travel time is almost unchanged. At this point, the capacity of the intersection, increased by reduced headways from AVs, is sufficient for the demand. Slight delays for a few vehicles are observed due to the randomness in the distribution of departure times and of AVs but overall the effect is small. This is consistent with the TBR/LEMITM model: the additional capacity required to reserve all turning movements for HV s is proportional to the percentage of HV . In practice, this may be used to predict the intersection delay for arbitrary proportions of AVs and thus determine the point at which TBR/LEMITM improves over signals. Of course, intersection delay also affects intersection demand through route choice, which is the subject of the DTA model of the rest of this section.

### 6.2. Shared road dynamic traffic assignment

We now consider a DTA model using the multiclass CTM and TBR/LEMITM intersection controls to study the predictions of the shared road model with DUE routing. The model was run on the downtown Austin network, which has 171 zones, 546 intersections, 1247 links, and 62836 trips, shown in Fig. 5. This network was chosen because many links are arterials or part of the downtown grid and terminate at (currently) signal-controlled intersections. Convergence was measured by comparing travel time with the shortest paths for 15 minute assignment intervals. Let $t_{r s t}^{*}$ be the travel time of the shortest path from $r$ to $s$ departing within $t \in \mathscr{T}$, where $\mathscr{T}$ is the set of all assignment intervals. Let $t_{v}$ be the travel time of vehicle $v$. The convergence measure of average excess cost (AEC) is then defined as

$$
\begin{equation*}
\mathrm{AEC}=\frac{\sum_{(r, s, t) \in Z^{2} \times \mathscr{F}} \sum_{v \in V_{r s} t} t(v)-t_{r s t}^{*}}{\sum_{(r, s, t) \in \mathcal{Z}^{2} \times \mathscr{F}}\left|V_{r s}\right|} \tag{27}
\end{equation*}
$$

where $Z$ is the set of zones and $V_{r s t}$ is the demand from $r$ to $s$ departing within $t \in \mathscr{T}$. DTA used the MSA solution algorithm (see Levin et al., 2014), but more complex techniques could improve convergence. Computation times for 50 iterations of MSA on an Intel Xeon processor running at 3.33 GHz are shown in Fig. 6. Since greater proportions of autonomous vehicles increase the network efficiency, and vehicles exit sooner, greater proportions of autonomous vehicles also decrease computation times. The computation times of less than 18 minutes per scenario allow a suite of scenarios to be run on the downtown Austin city network within a few hours.

### 6.3. Convergence

Fig. 7 shows the average excess cost per iteration for the $50 \%$ AVs scenario. The solution quickly reaches an AEC of less than 50 s , but the convergence pattern is slow and non-monotone afterward. However, that is expected for SBDTA (Levin et al., 2014).

Although convergence is difficult to prove for multiclass formulations even with static traffic assignment (Marcotte and Wynter, 2004), the multiclass DTA appears to converge to an equilibrium on the downtown Austin city network for all


Fig. 5. Downtown Austin network.


Fig. 6. Computation time with respect to proportion of AVs.


Fig. 7. Average excess cost for $50 \%$ AVs scenario.


Fig. 8. Total travel time as proportion of AVs increases.
studied proportions of AVs. These results empirically demonstrate that the multiclass dynamic flow and intersection models developed in this paper may be used with DTA on city networks.

### 6.4. Travel time predictions

Total travel time (TTT) with TBR/LEMITM are compared with traffic signals at intersections in Fig. 8. DTA was solved for each scenario, so vehicles are considering the average travel times from the correct AV proportion in their route choice. Traffic signals benefit from reduced headways for AVs but delay may be improved by TBR for 100\% AVs (Fajardo et al., 2011). However, this experiment explores the effects of these intersection controls for shared roads. The downtown Austin network (shown in Fig. 4) is mostly arterials and downtown grid region. Therefore intersections are the major source of congestion for many links. This is supported by the results: when traffic signals are used, TTT decreases only slightly. Although AVs increase capacity per signal phase, vehicles are still delayed waiting for a phase that allows their turning movement. In contrast, TBR/ LEMITM performs much worse when the proportion of AVs is low. For HVs, LEMITM is less efficient than signals because it reserves more of the intersection to ensure safe movement. However, intersection delay and TTT appear to decrease linearly at a significant rate with the proportion of AVs, as with the single intersection results in Section 6.1.

These results suggest that TBR/LEMITM improves over signals after AV penetration reaches around $80 \%$. However, the exact proportion of AVs at which TBR/LEMITM becomes advantageous may vary depending on the city network topology. Note that although Dresner and Stone (2007) and Bento et al. (2013) studied a single shared intersection, route choice may be affected by the proportion of AVs. Intersections with a higher proportion of AVs will experience lower delay and may encourage greater use. Therefore, to estimate the effect of intersection controls on route choice, a DTA framework such as the one presented here should be used.

## 7. Conclusions

Maturing AV technology suggests that AVs will be publicly available within the next few decades. To provide a framework for studying the effects of AVs on city networks, this paper develops a shared road DTA model for human and autonomous vehicles. A multiclass CTM is presented for vehicles traveling at the same speed with capacity and backwards wave speed a function of class proportions. A collision avoidance car following model incorporating vehicle reaction time is used to predict how reduced reaction times might increase capacity and backwards wave speed. These models are generalized to an arbitrary number of classes because different AVs may be certified for different reaction times. These models also use continuous flow so that SBDTA models built on continuous flows may incorporate these multiclass predictions.

The second part of a shared road DTA model is the intersection control. We modify the CR model proposed by Levin and Boyles (2015b) to include the LEMITM reservation model for non-AVs (Bento et al., 2013) while using conventional TBR for AVs. This TBR/LEMITM combination with multiclass CTM flow model is studied in a DTA framework on a single intersection and on a city network. Results verify that use of TBR/LEMITM decreases intersection delay linearly with the proportion of AVs, as is expected from the intersection model. This may be used to predict what AV penetration is required for TBR/ LEMITM to improve over traffic signals. Although results on downtown Austin suggest that $80 \% \mathrm{AV}$ penetration is required, this may depend on the network topology.

In future work, the capacity and backwards wave speed predicted here should be verified with microsimulation and/or real vehicles. Other such estimations may still be incorporated into the multiclass CTM model presented in this paper. The model of LEMITM should also be calibrated. On a larger scale, determining an efficient shared intersection controls is still an open question to bridge the gap between optimized traffic signals for HVs and TBR for AVs. New shared intersection controls may be implemented in this multiclass framework to study how their performance under DUE routing. This framework might also be used to study the impact of mixed intersection controls (some signals, some TBR/LEMITM) on DUE routing in a traffic network.

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## Appendix A. Supplementary material

Supplementary data associated with this article can be found, in the online version, at http://dx.doi.org/10.1016/j.trc. 2015.10.005.

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